

***PAST, PRESENT AND FUTURE
OF
EARTHQUAKE ANALYSIS OF STRUCTURES***

By Ed Wilson

September 22, 2014

SEAONC Lecture # 1

Summary of Lecture Topics

General Comments

Fundamental Principles of Mechanics and Nature

Methods of Dynamic Analysis and new Numerical Methods

Existing Problems with the Response Spectrum Method, RSM

Speed of Computers and New Numerical Methods

History of the SAP Series of Programs

Damping and Energy Dissipation

Recommendations on the RSM, by Ed and Others

The Life Story of Ed Wilson

Born in 1931 near Ferndale, CA – The Earthquake Capital of USA

Worked on a small ranch and in construction with my father

Moved to Sacramento in 1948 - After community college transferred to CAL for BS Degree in January 1955. 53-54 worked as Field Eng.

1955 – 56 Korea in the US Army

1957 – 63 Worked with Ray Clough for MS and D Eng

1963 – 65 Senior Research Engineer Aerojet - on the Apollo Project

1965 – 91 Teaching, Consulting and Research at CAL – 29 Docs

1981 – Started the development of SAP 80 for Personal Computers

1991 – Consulting and Computer Program Development SADSAP

Present ECRB 29 years CalTrans SAB 5 years Campus SRC

Professor Ray W. Clough

1938 First to Climb Several Cascade Mountains

1942 BS University of Washington, Civil Eng.

1943 - 1946 U. S. Army Air Force

1946 - 1949 MIT - D. Science - Bisplinghoff

1949 - 1986 Professor of CE U.C Berkeley

1952 and 1953 Summer Work at Boeing

National Academy of Engineering & Science

National Medal of Science



*To Ray Clough
Best Wishes*

Bill Clinton

Fundamental Equations of Structural Analysis

- 1. Equilibrium - Including Inertia Forces - Must be Satisfied*
- 2. Material Properties or Stress / Strain or Force / Deformation*
- 3. Displacement Compatibility Or Equations of Geometry*

Methods of Analysis

- 1. Force – Good for approximate hand methods*
- 2. Displacement - 99 % of programs use this method*
- 3. Mixed - Beam - Plane Sections & $V = dM/dz$*

Check Conservation of Energy

1964 Gene's Comment – a true story

- Ed developed a new program for the Analysis of Complex Rockets*

Ed talks to Gene -----

Two weeks later Gene calls Ed -----

Ed goes to see Gene -----

The next day, Gene calls Ed and tells him

***“Ed, why did you not tell me about this
program.***

It is the greatest program I ever used.”

Methods for the Earthquake Analysis of Linear Structures

Mode Superposition - *With Model Damping*

Step-By-Step Integration - *No Mode Shapes Needed*

With Rayleigh Damping and other Possible Numerical Problems

Frequency Domain – *Maybe good for Certain Problems*

Approximate Response Spectrum – *OK for one degree of freedom*

Methods for the Earthquake Analysis of Non-Linear Structures

Step-By-Step Integration - *No Mode Shapes Needed*

With Rayleigh Damping and other Possible Numerical Problems

- a. New Stiffness Matrix formed for each time step and iterate*
- b. In General, the high frequencies have large numerical damping.*

Fast Non-Linear Analysis Method *FNA Method and*

Using Load Dependent Ritz Vectors *LDR Vectors*

Over 20 years of very positive experience with very large structures

Speed, Accuracy, Error Evaluation and Conservation of Energy

My First Earthquake Engineering Paper

October 1-5 1962

SYMPOSIUM

OCTOBER

1-5 1962



ON THE USE OF

computers in civil engineering

Laboratório Nacional de Engenharia Civil

Lisbon - Portugal

PAPER Nº.45

DYNAMIC RESPONSE BY STEP-BY-STEP MATRIX

ANALYSIS

by

Edward L. Wilson¹ and Ray W. Clough²

THE PRESENT

*Comments on the
Response Spectrum Analysis Method*

SEISMIC DESIGN CRITERIA

As used by

Many Large Engineering Groups

Topics

1. Why do most Engineers have Trouble with Dynamics?

Taught by people who love math – No physical examples

2 Who invented the Response Spectrum Method?

Ray Clough and I did – by putting it into my computer program

3 Application to “Ordinary Standard Structures”

Why 30 ? Why reference to Transverse & Longitudinal directions?

4 Physical behavior of Skew Bridges – Failure Mode

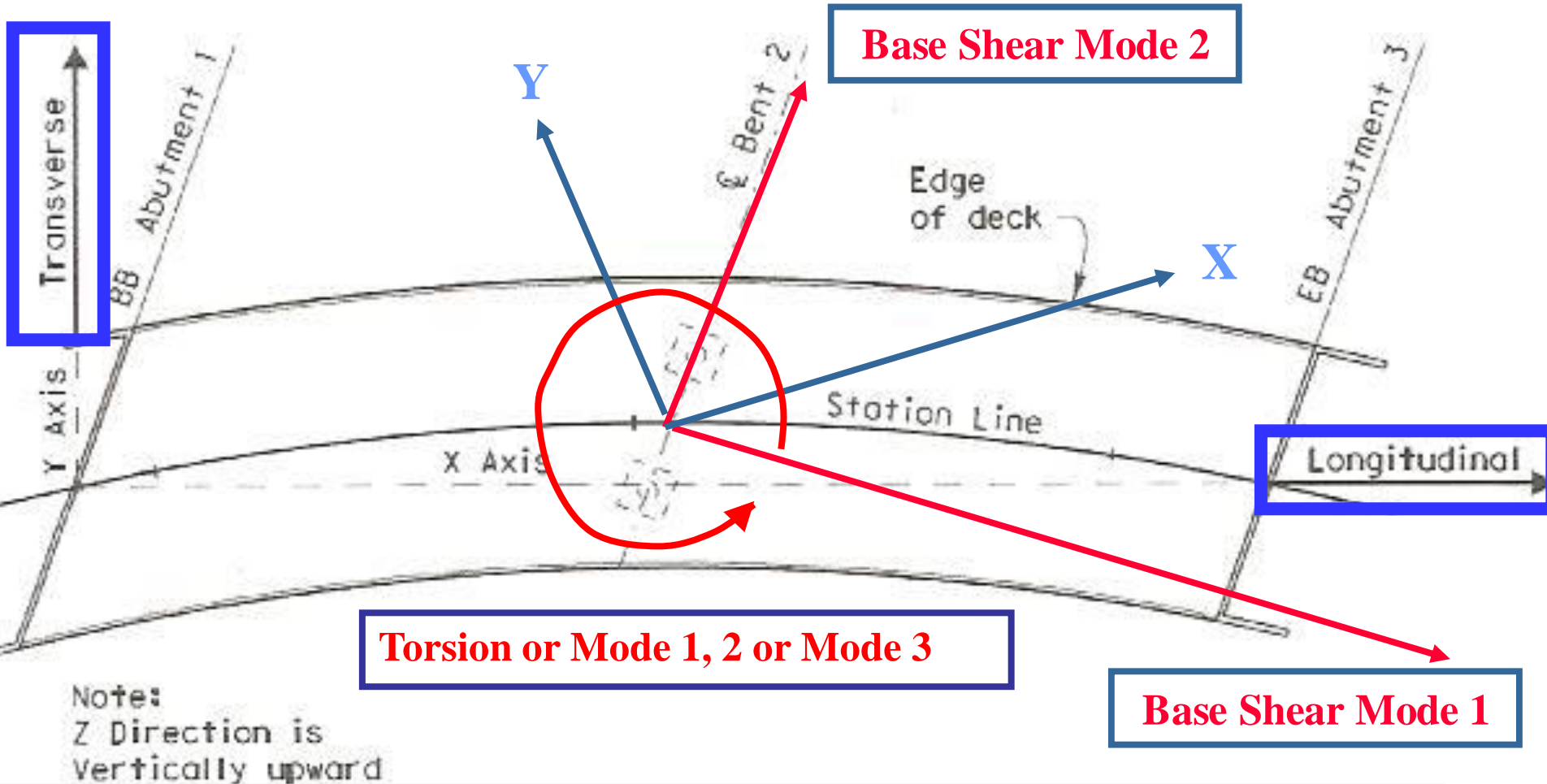
5 Why use the 1960 Equal Displacement Rule?

6 Quote from George W. Housner

Who Developed the Approximate Response Spectrum Method of Seismic Analysis of Bridges and other Structures?

- 1. Fifty years ago there were only digital acceleration records for 3 earthquakes.*
- 2. Building codes gave design spectra for one degree of freedom systems with no guidance of how to combine the response of the higher modes.*
- 3. At the suggestion of Ray Clough, I programmed the square root of the sum of the square of the modal values for displacements and member forces. However, I required the user to manually combine the results from the two orthogonal spectra. Users demanded that I modify my programs to automatically combine the two directions. I refused because there was no theoretical justification.*
- 4. The user then modified my programs by using the 100%+30% or 100%+40% rules.*
- 5. Starting in 1981 Der Kiureghian and I published papers showing that the CQC method should be used for combining modal responses for each spectrum and the two orthogonal spectra be combined by the SRSS method.*
- 6. We now have Thousands or of 3D earthquake records from hundreds of seismic events. Therefore, why not use Linear or Nonlinear Time-History Analyses that SATISFIES FORCE EQUILIBRIUM at every point in time.*

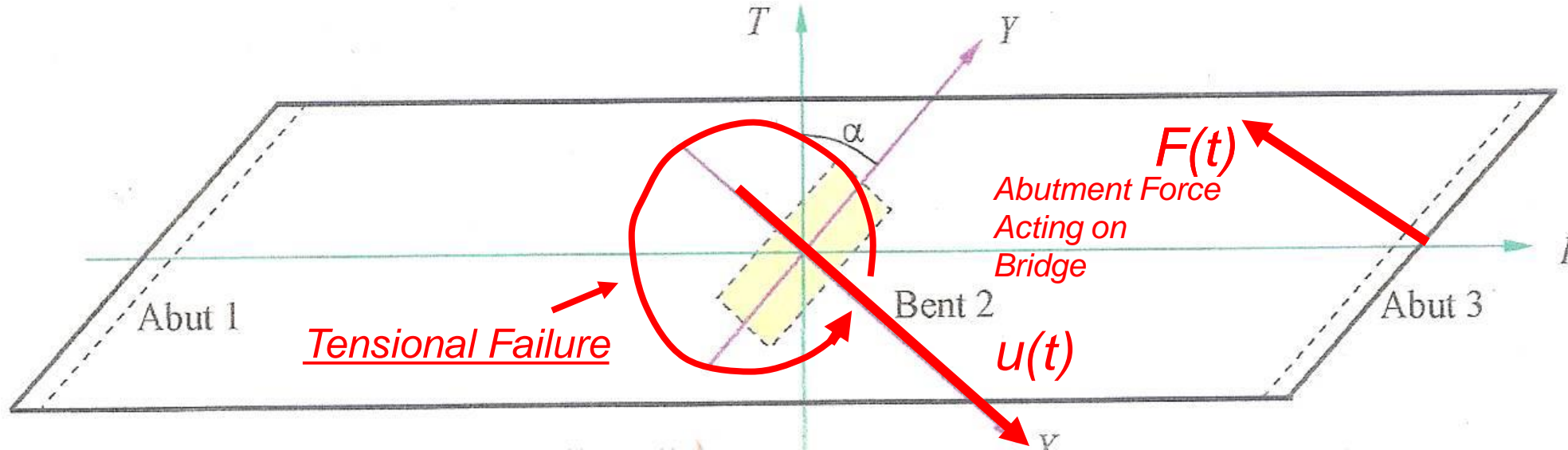
If Equal Spectra are applied to any Global X-Y-Z System



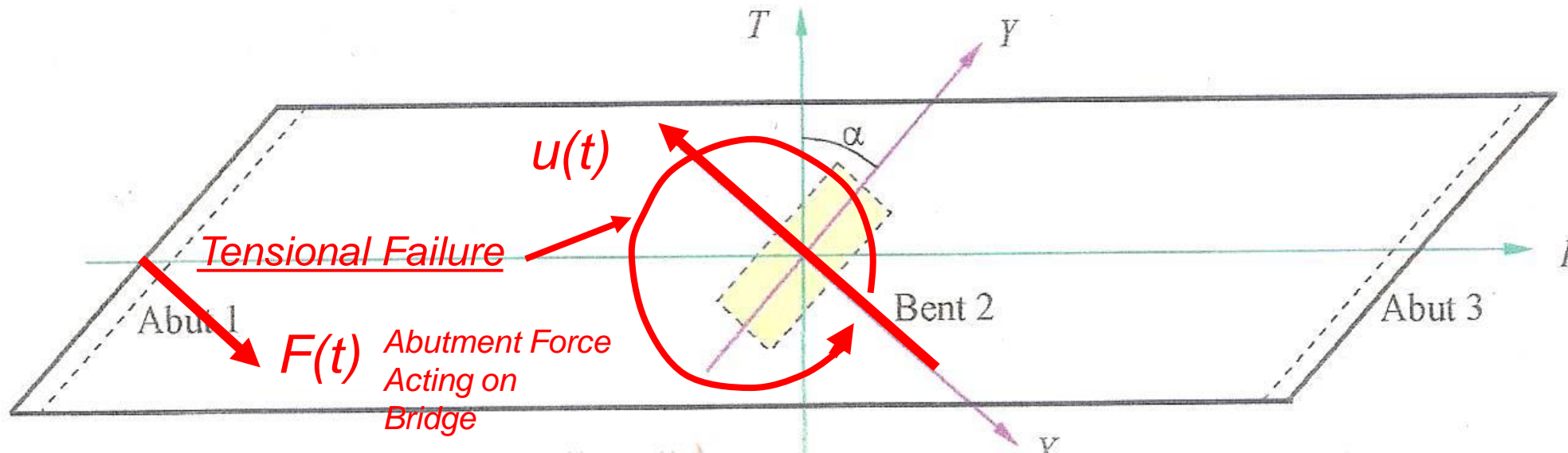
Member Forces are the same for all Global X-Y Systems,

If Calculated from
$$F_i = \sqrt{F_{iX}^2 + F_{iY}^2 + F_{iZ}^2}$$

Nonlinear Failure Mode For Skew Bridges

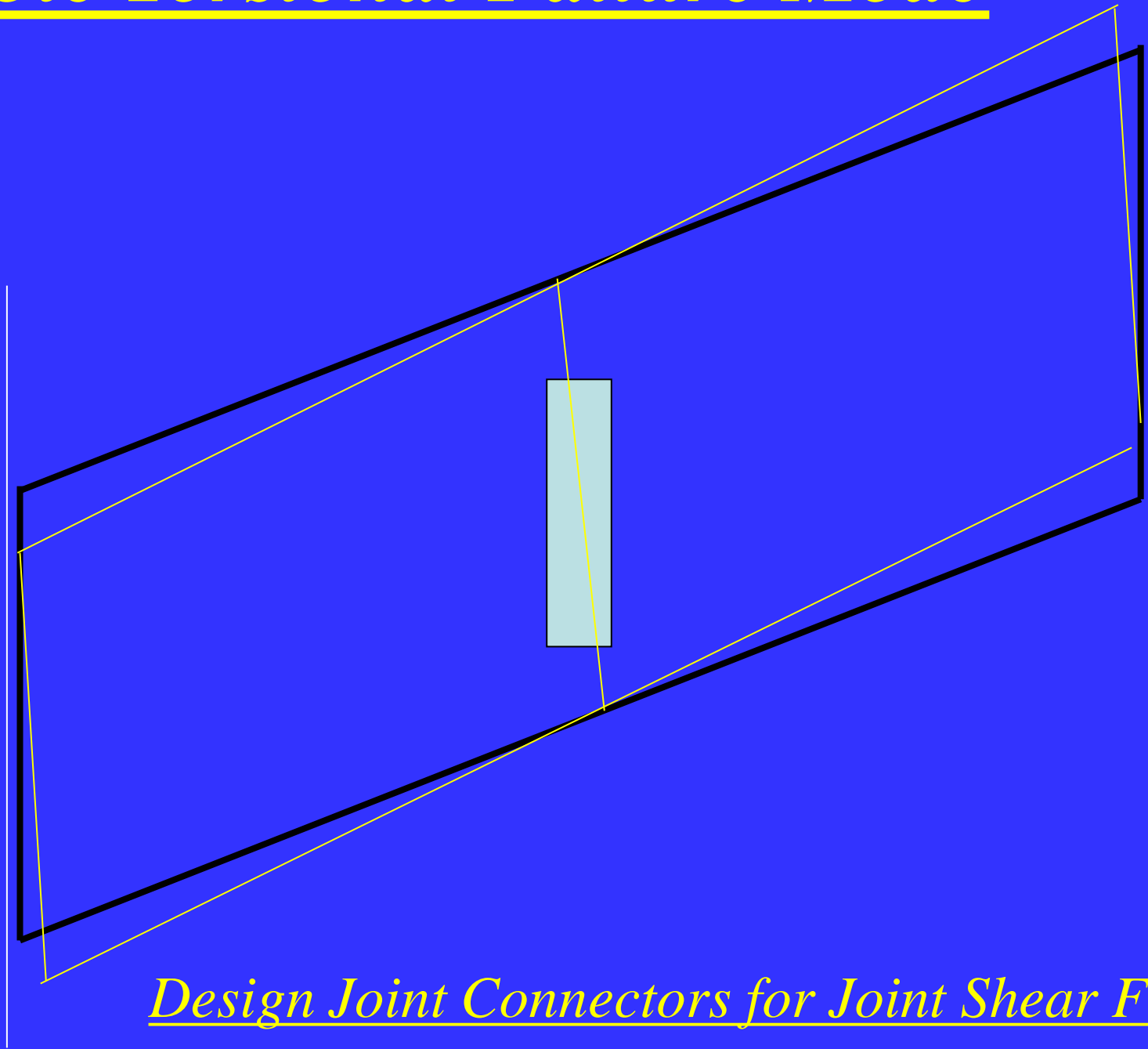


Contact at Right Abutment



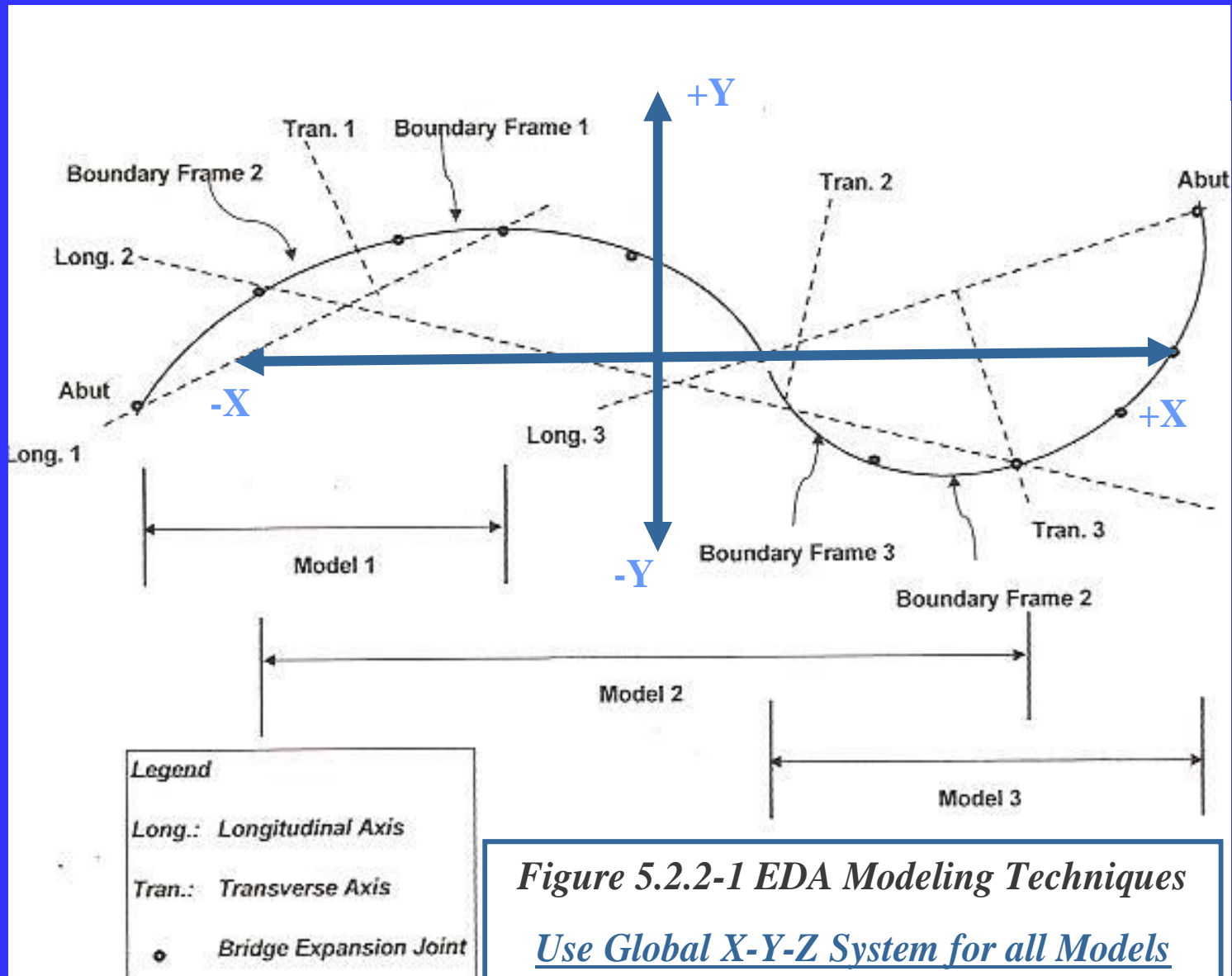
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Possible Torsional Failure Mode



Design Joint Connectors for Joint Shear Forces !

Use a Global Modal for all Analyses



Equal Displacement Rule

In 1960 Veletsos and Newmark proposed in a paper presented at the 2nd WCEE in Japan

For a one DOF System, subjected to the El Centro Earthquake, the Maximum Displacement was approximately the same for both linear and nonlinear analyses.

In 1965 Clough and Wilson, at the 3rd WCEE in Chile, proved the Equal Displacement Rule did not apply to multi DOF structures.

See edwilson.org to read paper.

1965 Professor Clough's Comment

“The maximum displacements from a nonlinear a dynamic analysis are significantly greater than the displacements obtained from a linear dynamic analysis”

2014 Comment by Old Ed Wilson

“Today, It appears the earthquake displacements at bridge joints are being predicted by the
Equal Displacement Rule”

1965 Comments by Ray and Ed

“If tall buildings are designed for elastic column behavior and restrict the nonlinear bending behavior to the girders, it appears the danger of total collapse of the building is reduced.”

This indicates the strong-column and weak beam design is the one of the first statements on

Performance Based Design

Comment on the use of the Response Spectrum Method

I do not know who first called it a “response spectrum,” but unfortunately the term leads people to think that it characterizes the building’s motion, rather than the ground’s motion.

George W. Housner

EERI Oral History, 1996

Seismic Analysis Advice by Ed Wilson

- 1. All Structures Bridges are Three-Dimensional and their Dynamic Behavior is governed by the Mass and Stiffness Properties of the structure. The Longitudinal and Transverse directions are geometric properties. All Structures have Torsional Modes of Vibrations.*
- 2. The Response Spectrum Analysis Method is a very approximate method of seismic analysis which only produces positive values of displacements and member forces which are not in equilibrium. Demand -Capacity Ratios have Very Large Errors*
- 3. Short and Long Duration earthquakes are treated by using the same “Design Spectra”. Results are maximum probable values and occur at an “Unknown Time”.*
- 4. The Engineer does not gain insight into the “Dynamic Behavior of the Structure”*

“Linear Dynamic Response Analysis”

It is a simple extension of Static Analysis – just add mass and time dependent loads

- 1. Static and Dynamic Equilibrium is satisfied at all points in time if all modes are included*
- 2. Errors in the results can be estimated automatically if modes are truncated*
- 3. Time-dependent plots and animation are impressive and fun to produce*
- 4. Demand /Capacity Ratios are accurate and a function of time – summarized by program.*
- 5. Engineers can gain great insight into the dynamic response of the structure and may help in the redesign of the structural system.*

Convince Yourself with a simple test problem

- 1. Select an existing Sap 2000 model of an Ordinary Standard Bridge with several different spans – both straight and curved.*
- 2. Select a 3D earthquake ground acceleration record to be used as the input loading which is approximately 20 seconds long.*
- 3. Create a spectra from the selected earthquake ground acceleration record.*
- 4. Using a number of modes that captures a least 90 percent of the mass in all three directions.*
- 5. At any angle, Run a Linear Time History Analysis and a Response Spectrum Analysis.*
- 6. Compare Demand Capacity Ratios for both SAP 2000 analyses for all members.*
- 7. You decide if the Approximate RSA results are in good agreement with the Linear time History Results.*

End of Bridge Lecture

Teaching

Casper, Phillips and Associates in Tacoma

Nonlinear Dynamic Analysis

Over the Telephone

In Six Weeks

Response Spectrum Method

Basic Equations in Earthquake Engineering

$$m\ddot{u}_a(t) + c\dot{u}_r(t) + ku_r(t) = 0$$

Basic Assumption in Eq. Eng. $\ddot{u}_a = \ddot{u}_g + \ddot{u}_r$

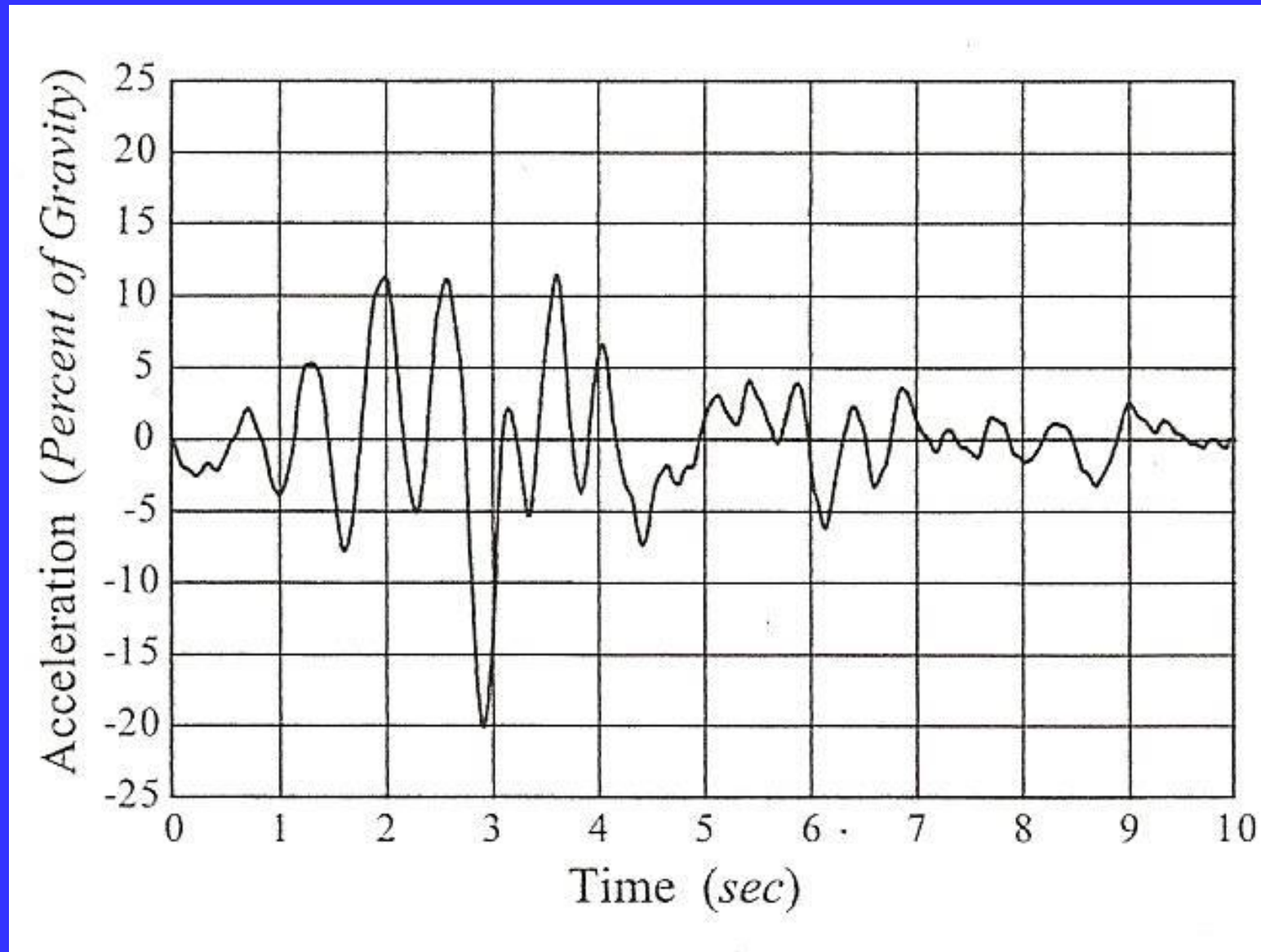
$$m\ddot{u}_r(t) + c\dot{u}_r(t) + ku_r(t) = -mu_g(t)$$

This assumes a rigid foundation and structure.

In the real world, which we all live in, the horizontal Earthquake Displacements Propagate from the foundation Upward into the Structure.

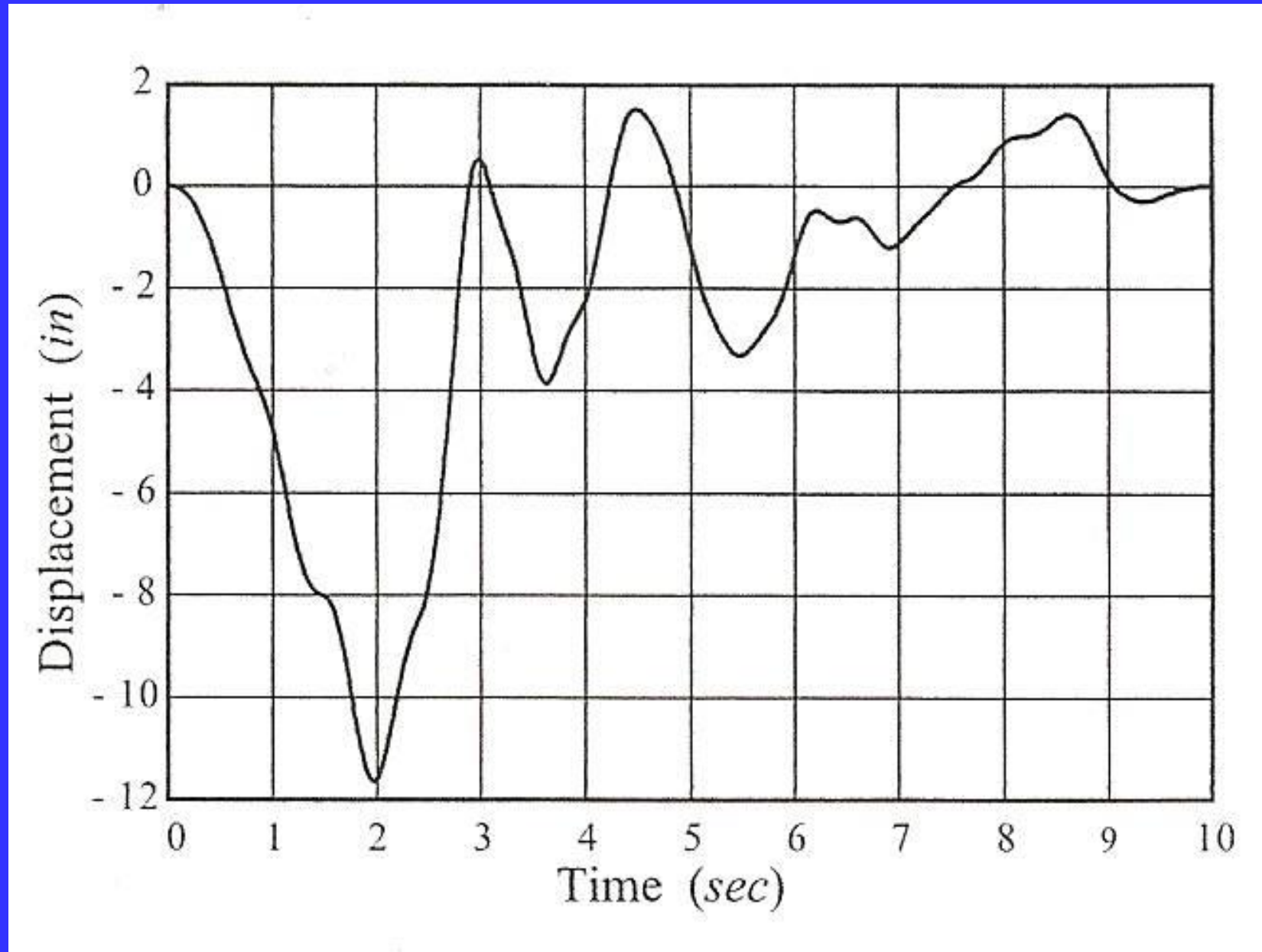
WHY DO WE DO A PUSHOVER ANALYSIS?

How we Calculate a Response Spectra Today

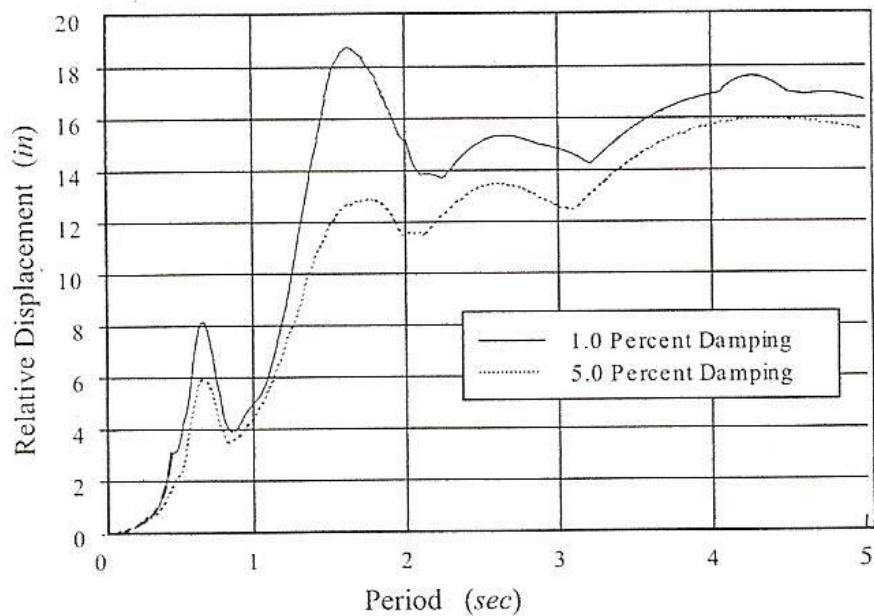


Typical Earthquake Ground Acceleration – percent of gravity

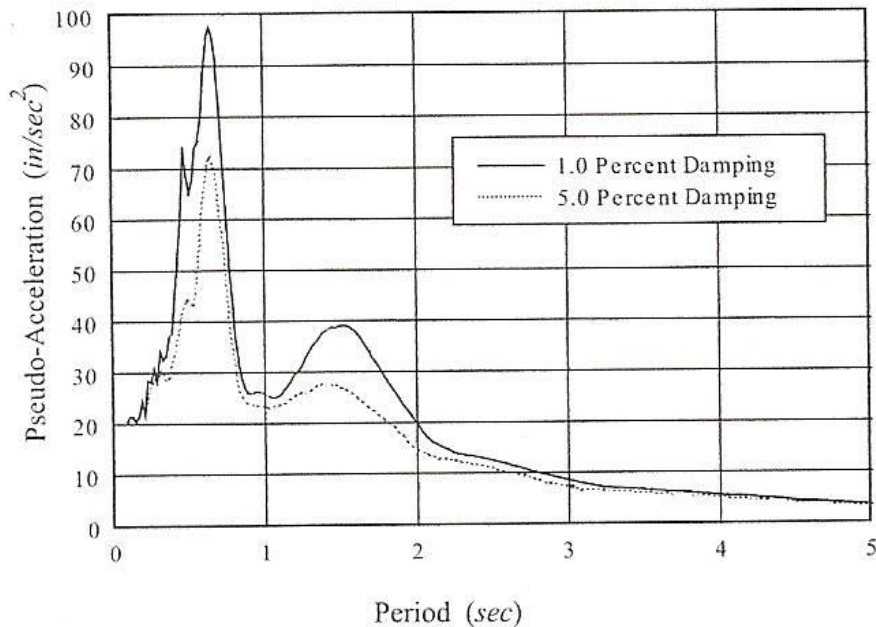
Integration will produce Earthquake Ground Displacement – inches



These real Eq. Displacement can be used as Computer Input



(a) Relative Displacement Spectrum, $y_{\max}(\omega)$



(b) Pseudo-Acceleration Spectrum, $S_a = \omega^2 y_{\max}(\omega)$

Relative Displacement Spectrum for a unit mass with different periods

1. These displacements u_{\max} are maximum (+ or -) values versus period for a structure or mode.
2. Note: we do not know the time these maximums took place.

Pseudo Acceleration Spectrum

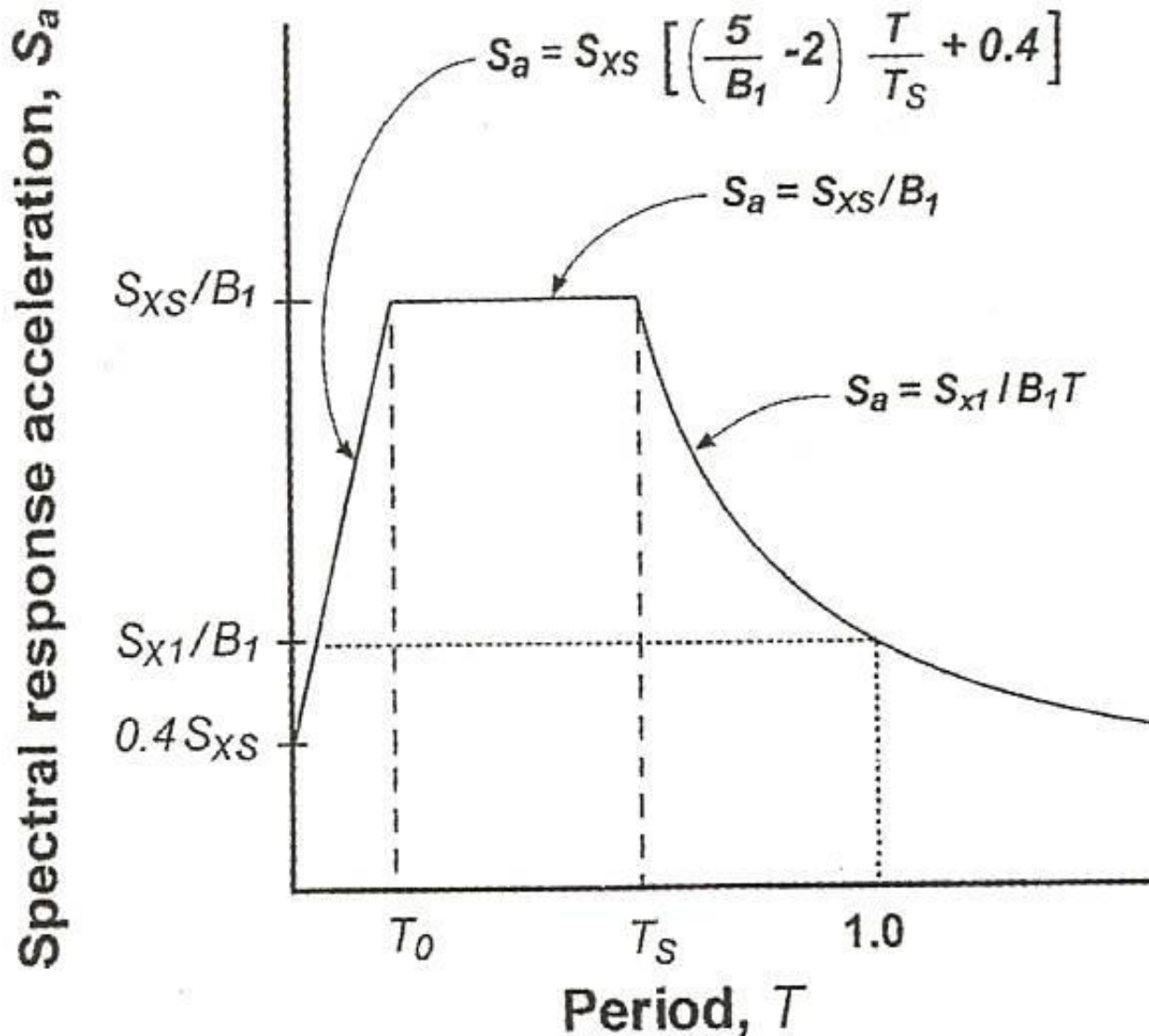
Note: $S = \omega^2 u_{\max}$ has the same properties as the Displacement Spectrum. Therefore, how can anyone justify combining values, which occur at different times, and expect to obtain accurate results.

Random Vibrations?

$t = \pm \text{infinity}$ Also site effects

General Horizontal Response Spectrum

from ASCE 41-06



Simple User Defined Data

β = effective viscous ratio

S_{XS} = peak base acceleration

S_{X1} = value at 1.0 sec period

Constants to be Calculated

$$B_1 = 4[5.6 - \ln(100\beta)]$$

$$T_S = S_{X1} / S_{SX}$$

$$T_0 = 0.2T_S$$

Duration has been Neglected

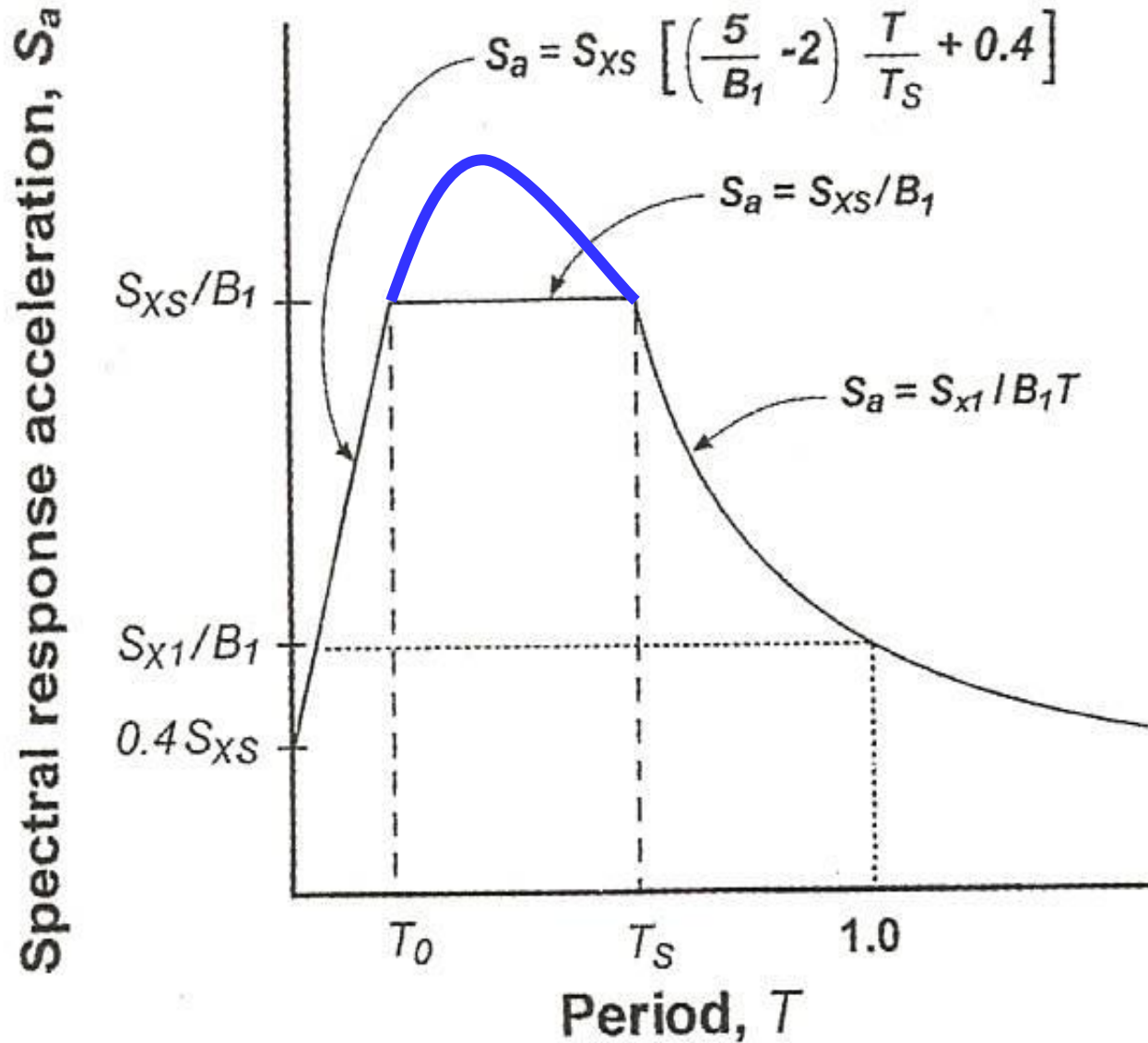
Shape is not Realistic

NonLinear Structures - No

Where did the hat go?

Where did the Hat go - on the Response Spectrum ?

As I Recall -----



Demand-Capacity Ratios

The Demand-Capacity ratio for a linear elastic compression member is given by an equation of the following general form:

$$R(t) = \frac{|P(t)|}{\phi_c P_{cr}} \pm \frac{M_2(t) C_2}{\phi_b M_{c2} \left(1 - \frac{|P(t)|}{P_{e2}}\right)} \pm \frac{M_3(t) C_3}{\phi_b M_{c3} \left(1 - \frac{|P(t)|}{P_{e3}}\right)} \leq 1.0$$

If the axial force and the two moments are a function of time, the Demand-Capacity ratio will be a function of time and a smart computer program will produce $R(\max)$ and the time it occurred.

A smart engineer will hand check several of these values.

RSM Demand-Capacity Ratios

If the axial force and the two moments are produced by the Response Spectrum Method the Demand-Capacity ratio may be computed by an equation of the following general form:

$$R(max) = \frac{|P(max)|}{\phi_c P_{cr}} + \left| \frac{M_2(max)C_2}{\phi_b M_{c2} \left(1 - \frac{|P(max)|}{P_{e2}}\right)} \right| + \left| \frac{M_3(max)C_3}{\phi_b M_{c3} \left(1 - \frac{|P(max)|}{P_{e3}}\right)} \right| \leq 1.0$$

Structural Analysis Programs can compute and display this Demand-Capacity Ratio.

However, anyone who believes it does not have

Common Sense

SPEED and COST of COMPUTERS

1957 to 2014 to the Cloud

*1957 My First Computer in Cory Hall
IBM 701 Vacuum Tube Digital Computer
Could solve 40 equations in 30 minutes*



*In 1959 the campus got a IBM 704 with Floating Point hardware
and more fast memory – it was a joy to program*

1981 My First Computer Assembled at Home

Paid \$6000 for a 8 bit CPM Operating System with FORTRAN.

Used it to move programs from the CDC 6400 to the VAX on Campus.

Developed a new program called SAP 80 without using any Statements from previous versions of SAP.

After two years, system became obsolete when IBM released DOS with floating point chip.

In 1984, CSI developed Graphics and Design Post-Processor and started distribution of the Professional Version of Sap 80



Floating-Point Speeds of Computer Systems

Definition of one Operation $A = B + C * D$ 64 bits - REAL*8

Year	Computer or CPU	Operations Per Second	Relative Speed
1963	CDC-6400	50,000	1
1964	CDC-6600	100,000	2
1974	CRAY-1	3,000,000	60
1981	IBM-3090	20,000,000	400
1981	CRAY-XMP	40,000,000	800
1994	Pentium-90	3,500,000	70
1995	Pentium-133	5,200,000	104
1995	DEC-5000 upgrade	14,000,000	280
1998	Pentium II - 333	37,500,000	750
1999	Pentium III - 450	69,000,000	1,380

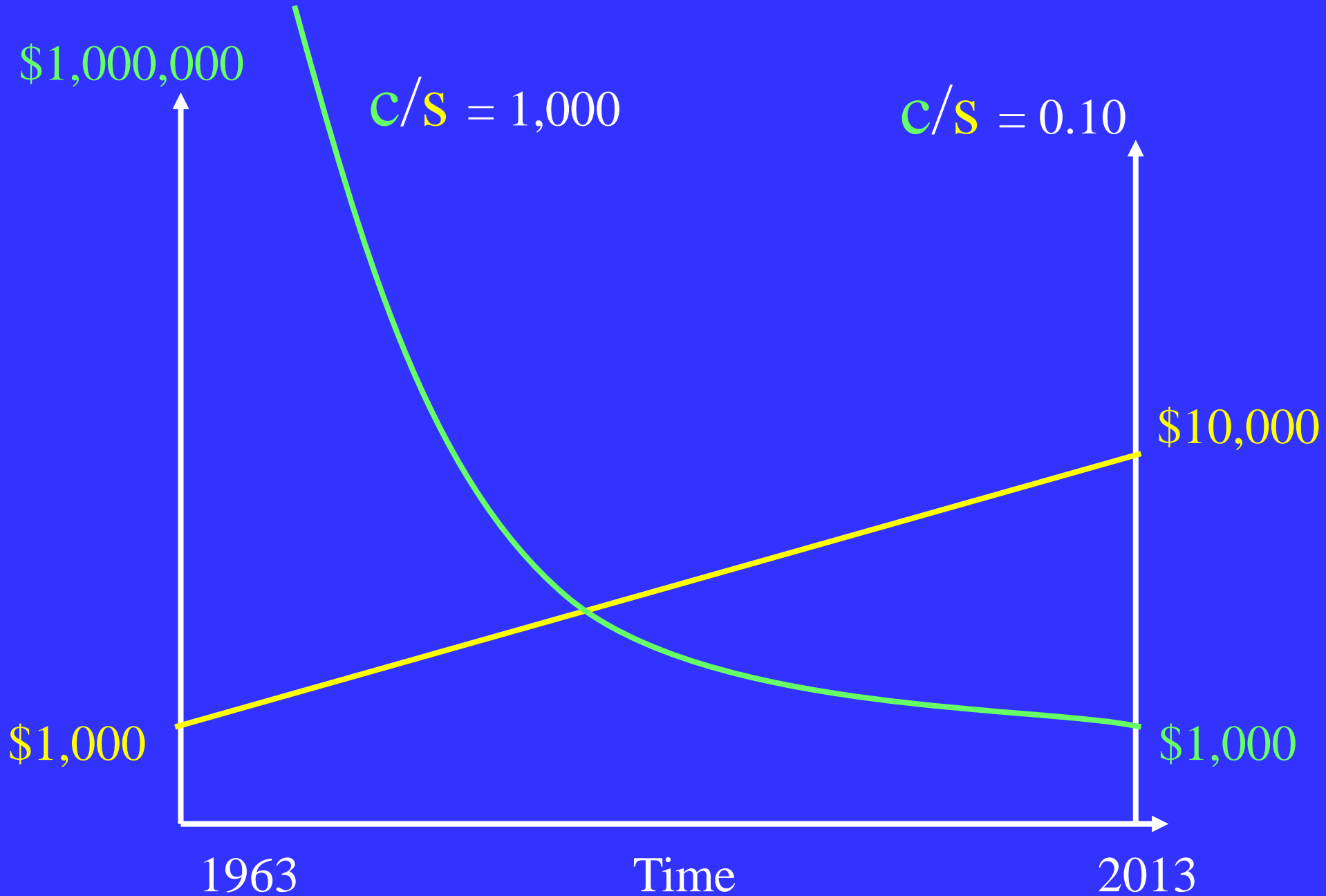
Cost of Personal Computer Systems

YEAR	CPU	Speed MHz	Operations Per Second	Relative Speed	COST
1980	8080	4	200	1	\$6,000
1984	8087	10	13,000	65	\$2,500
1988	80387	20	93,000	465	\$8,000
1991	80486	33	605,000	3,025	\$10,000
1994	80486	66	1,210,000	6,050	\$5,000
1996	Pentium	233	10,300,000	52,000	\$4,000
1997	Pentium II	233	11,500,000	58,000	\$3,000
1998	Pentium II	333	37,500,000	198,000	\$2,500
1999	Pentium III	450	69,000,000	345,000	\$1,500
2003	Pentium IV	2000	220,000,000	1.100,000	\$2.000
2006	AMD - Athlon	2000	440,000,000	2,200,000	\$950

<i>Year</i>	<i>Computer or CPU</i>	<i>Cost</i>	<i>Operations Per Second</i>	<i>Relative Speed</i>
1963	CDC-6400	\$1,000,000	50,000	1
1974	CRAY-1	\$4,000,000	3,000,000	60
1981	VAX or Prime	\$100,000	100,000	2
1994	Pentium-90	\$5,000	4,000,000	70
1999	Intel Pentium III-450	\$1,500	69,000,000	1,380
2006	AMD 64 Laptop	\$2,000	400,000,000	8,000
2009	Min Laptop	\$300	200,000,000	4,000
2010	2.4 GHz Intel Core i3 64 bit Win 7 Laptop	\$1,000	1.35 Billion Intel Fortran	27,000
2013	2.80 GHz 2 Quad Core 64 bit Win 7	\$1,000	2.80 Billion Parallelized Fortran	56,000

The cost of one operation has been reduced by 56 Billion in the last 50 years

Computer Cost versus Engineer's Monthly Salary



*NOW - You can now buy a very
Fast computer for less than \$1,000*

However

If it has a new operating system

*It may cost you Several thousand dollars
of your time to learn how to use all the new
options.*

*Also, you will need to buy new computer
Software from Microsoft*

SPEED

*60 years ago
April 17, 1954*

*Cal vs UCLA
Track Meet*

*Ed set a meet Record
in the 880 Yd Race*

*UC President
Robert G Sproul
held the tape*



SAP

STRUCTURAL ANALYSIS PROGRAM

ALSO A PERSON

“Who Is Easily Deceived Or Fooled”

“Who Unquestioningly Serves Another”

From The Foreword Of The First SAP Manual

"The slang name S A P was selected to remind the user that this program, like all programs, lacks intelligence.

It is the responsibility of the engineer to idealize the structure correctly and assume responsibility for the results."

Ed Wilson 1970

The SAP Series of Programs

<i>1969 - 70</i>	<i>SAP</i>	<i>Used Static Loads to Generate Ritz Vectors</i>
<i>1972 -73</i>	<i>SAP IV</i>	<i>Subspace Iteration – Dr. Jürgen Bathe</i>
<i>1973 – 74</i>	<i>NON SAP</i>	<i>New Program – The Start of ADINA</i> <u><i>Gave FORTRAN programs away</i></u>
<i>1980 – 82</i>	<i>SAP 80</i>	<i>New Linear Program for Personal Computers</i>

Lost All Research and Development Funding

<i>1983 – 1987</i>	<i>SAP 80</i>	<i>CSI added Pre and Post Processing</i>
<i>1987 - 1990</i>	<i>SAP 90</i>	<i>Significant Modification and Documentation</i>
<i>1997 – 2000</i>	<i>SAP 2000</i>	<i>Nonlinear Elements – More Options –</i> <i>With Windows Interface</i>
<i>2001 - Ed stopped</i>	<i>development work</i>	<i>– could not adjust to Windows</i>
<i>2014 – CSI</i>	<i>Continues to improve programs</i>	<i>with creativity</i>

Damping and Energy Dissipation

Inelastic Materials – *Dissipation of Strain Energy*

Friction – *Energy loss proportional to displacements*

Radiation – *Kinetic and Strain Energy within a Vibrating Structure is Transferred to the Foundation*

Linear Viscous Damping – *Does not exist in any human made device. Or f_d is not equal to $c\dot{u}$*

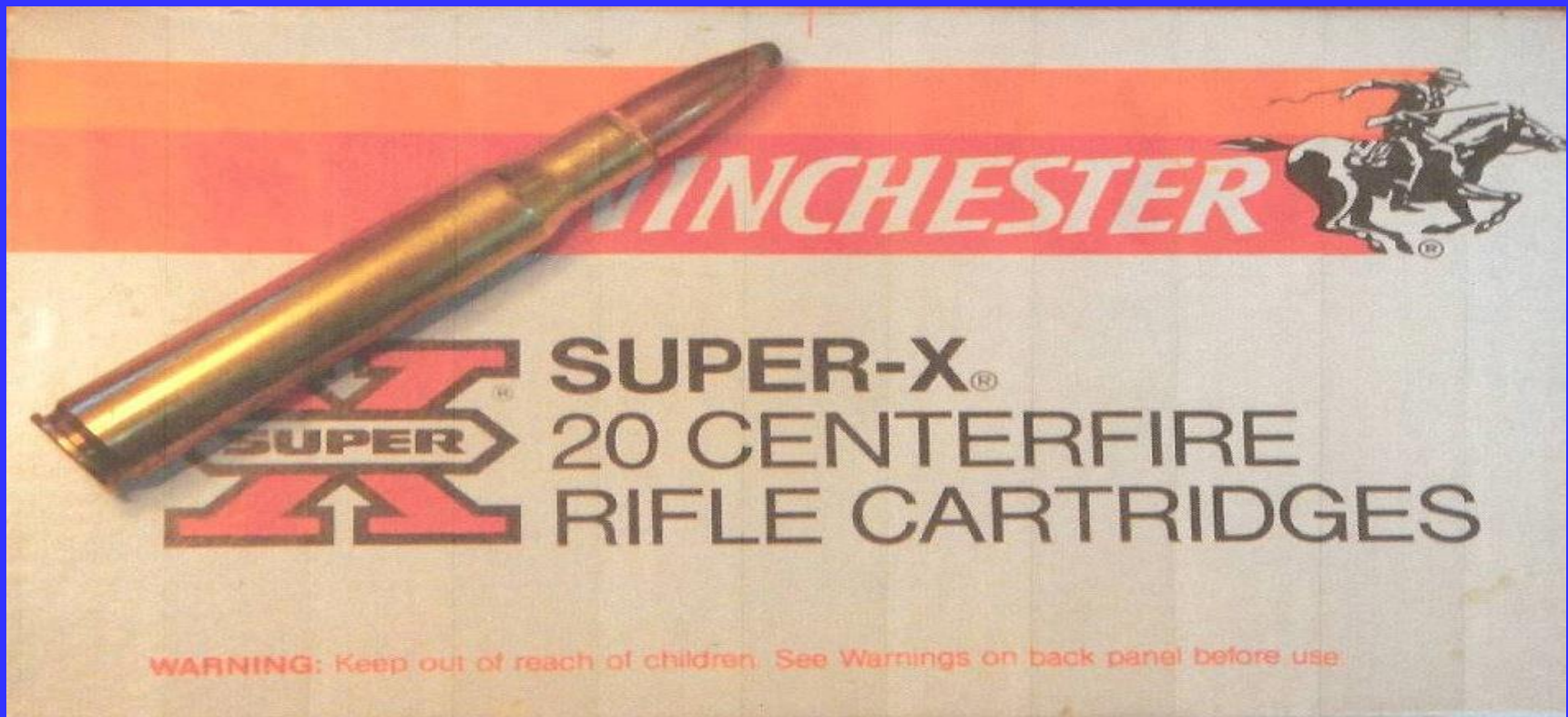
Therefore, the use of Complex Variable Notation is not necessary in dynamic analysis.

Structures Fail due to Strain Energy not Kinetic Energy



Best design will have minimum Strain Energy?

*This type of Kinetic Energy can Kill
Several Million times more people than
Earthquakes*



Terminology in nonlinear analysis
Which does not have a unique definition

- 1. Equal Displacement Rule*
- 2. Pushover Analysis*
- 3. Equivalent Linear Damping*
- 4. Equivalent Static Analysis*
- 5. Nonlinear Spectrum Analysis*
- 6. Onerous Response History Analysis*

Approximations are Necessary

However:

- 1. Do not use a 1960 rule without verification.*
- 2. There is always a more accurate method to solve a problem.*
- 3. If a large organization uses a method it does not make it a correct method.*
- 4. After you complete a large analysis, do parameter studies, or, use another method to analyze the structure . *There are 168 hours in a week.**

Recommendations – slide 1

Proposed by Ed Wilson and many others & ATC-82 Project

Let us be realistic, the majority of our engineering colleagues want to use the RSM; and, we will respect their decisions.

Therefore, we will propose an “optional” alternative to the use of the response spectrum method.

The design engineer will be allowed to use ‘three dimensional time-history records’ if their spectra exceeds the code values for all periods.

These “spectrally matched earthquake motions” must be based on modified recorded earthquake records.

Recommendations – slide 2

In addition, the maximum component of the three dimensional earthquake records must be applied in the most flexible direction of the structure, as defined by the direction of the base shear associated with the lowest frequency of the structure.

The same earthquake must be applied at 90 degrees to the first analysis.

*Also, two additional **spectrally matched earthquake motions** of different durations must be used in two additional analyses.*

Recommendations – slide 3

Add + and - 5 percent static torsion load.

In order to include P-Delta analysis the geometric stiffness, due to vertical dead loads, will be included in the calculation of mode shapes and frequencies.

We believe, after a smart structural engineer does these six analyses and compares the results with the standard RSM, it will be apparent a superior and less expensive design has been produced.

These results will satisfy all existing Codes - NOW!

Thank you

1963 Nonlinear story